

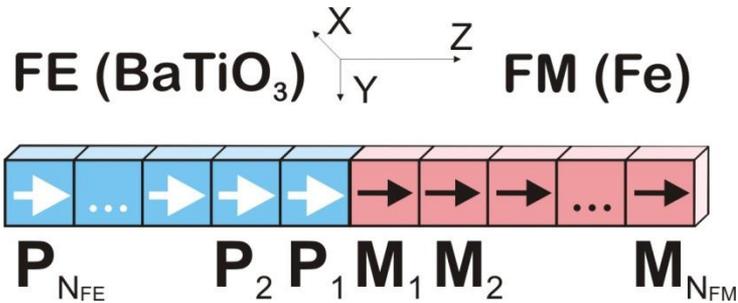
Electromagnetically controlled Multiferroic thermal diode

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- Composite two phase multiferroics
- Zero temperature Ferroelectric/Ferromagnetic solitons
- Multiferroic thermal diode

Magnetolectric coupling two phase multiferroics



$$F_{\Sigma} \sim a_{FE}^3 F_{FE} + a_{FM}^3 F_{FM} + E_C$$

Landau-Khalatnikov equation

$$\gamma_v \frac{d\mathbf{P}_i}{dt} = - \frac{\delta F_{\Sigma}}{\delta \mathbf{P}_i}$$

Screening effect and magnetolectric coupling

$$V_{ME} = -g_1 (P_N M_{N+1}^z) - g_2 (P_N M_{N+1}^z)^2$$

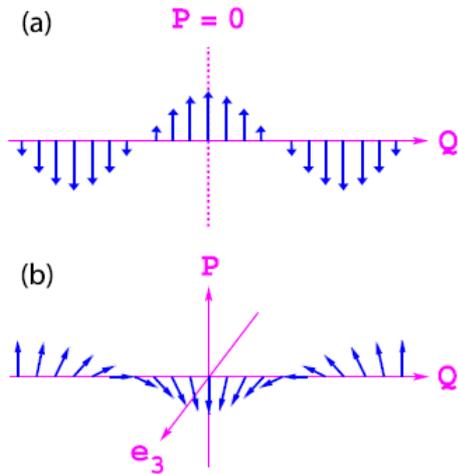
Landau-Lifshitz-Gilbert equation

$$\frac{d\mathbf{M}_j}{dt} = - \frac{\gamma}{1 + \alpha_{FM}^2} \left[\mathbf{M}_j \times \mathbf{H}_j^{\text{eff}}(t) \right] - \frac{\alpha_{FM} \gamma}{1 + \alpha_{FM}^2} \frac{1}{M_S} \left[\mathbf{M}_j \times \left[\mathbf{M}_j \times \mathbf{H}_j^{\text{eff}}(t) \right] \right]$$

$$\mathbf{H}_j^{\text{eff}}(t) = -\delta F_{\Sigma} / \delta \mathbf{M}_j$$

C.-L. Jia, T.-L. Wei, C.-J. Jiang, D.-S. Xue, A. Sukhov, and J. Berakdar Phys. Rev. B **90**, 054423 (2014);
L. Chotorlishvili, S. R. Etesami, and J. Berakdar R. Khomeriki, Jie Ren, Phys. Rev. B **92**, 134424 (2015)

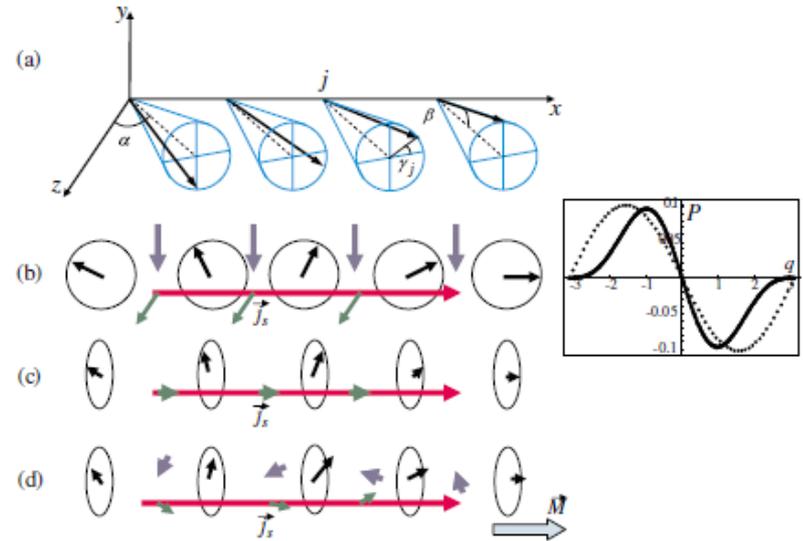
Magnetolectric coupling single phase multiferroics



S. W. Cheong and M. Mostovoy, Nat. Mater. **6**, 13 (2007);
 M. Mostovoy, Phys. Rev. Lett. **96**, 067601 (2006).

The sinusoidal spin wave does not induce
 a electric polarization **but Helicoidal does**

$$\vec{P} = \gamma \chi_e \left[(\vec{M} \cdot \vec{\nabla}) \vec{M} - \vec{M} (\vec{\nabla} \cdot \vec{M}) \right]$$

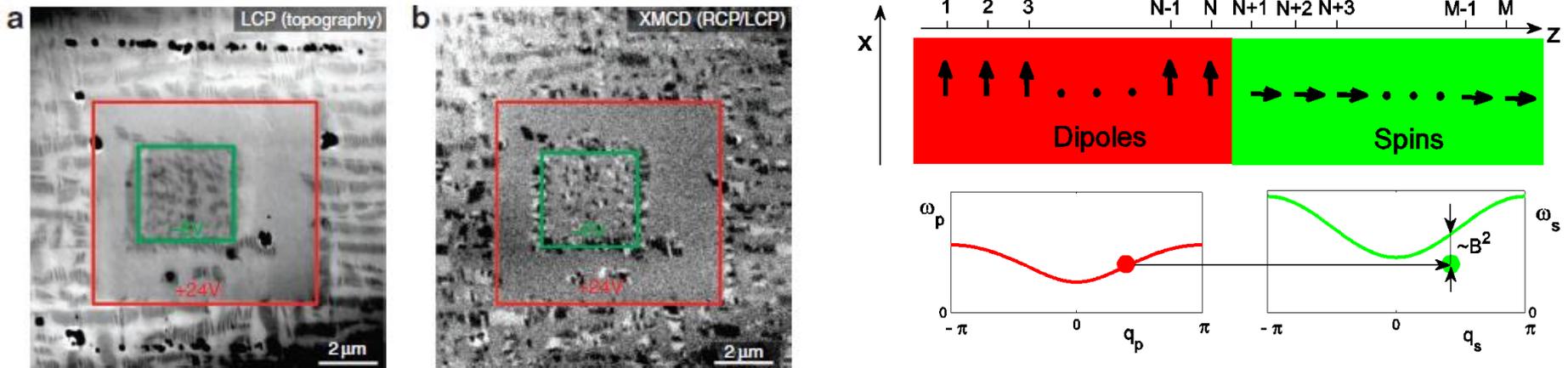


H. Katsura, N. Nagaosa, and Alexander V.
 Balatsky Phys. Rev. Lett. **95**, 057205 (2005);

$$V_{ME} = -\vec{E} \vec{P}$$

$$\vec{P} \sim \vec{e}_{i,i+1} \times (\vec{S}_i \times \vec{S}_{i+1})$$

Electrical control of magnetism two phase multiferroics $BaTiO_3Fe$



Hamiltonian of model: *Coarse-grained approach for system*
Ginzburg-Landau-Devonshire (GLD) potential

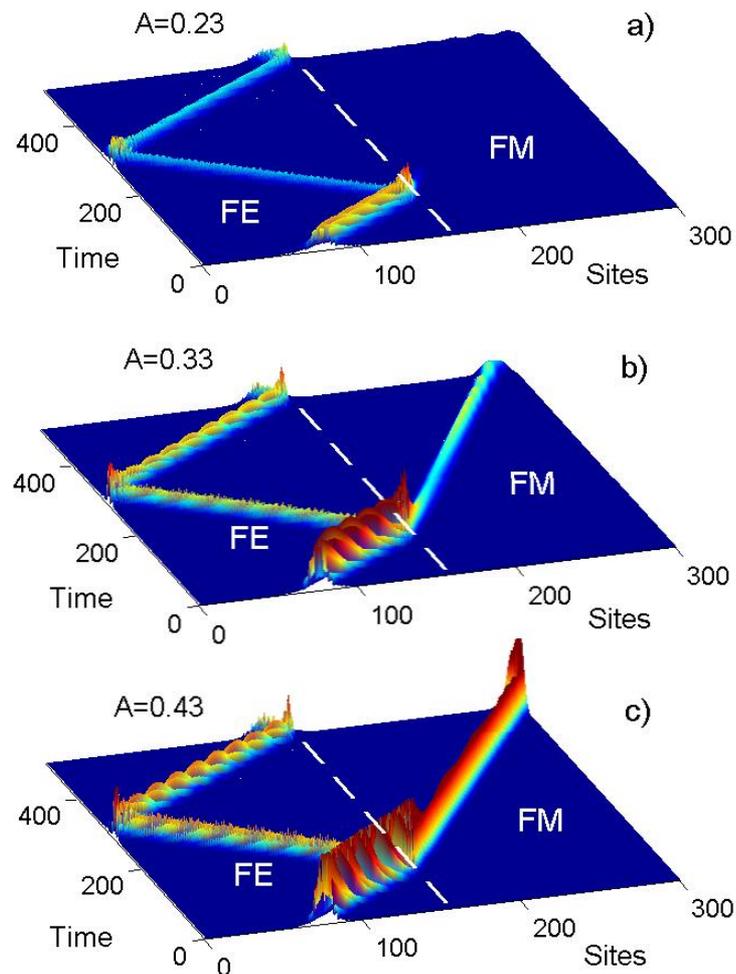
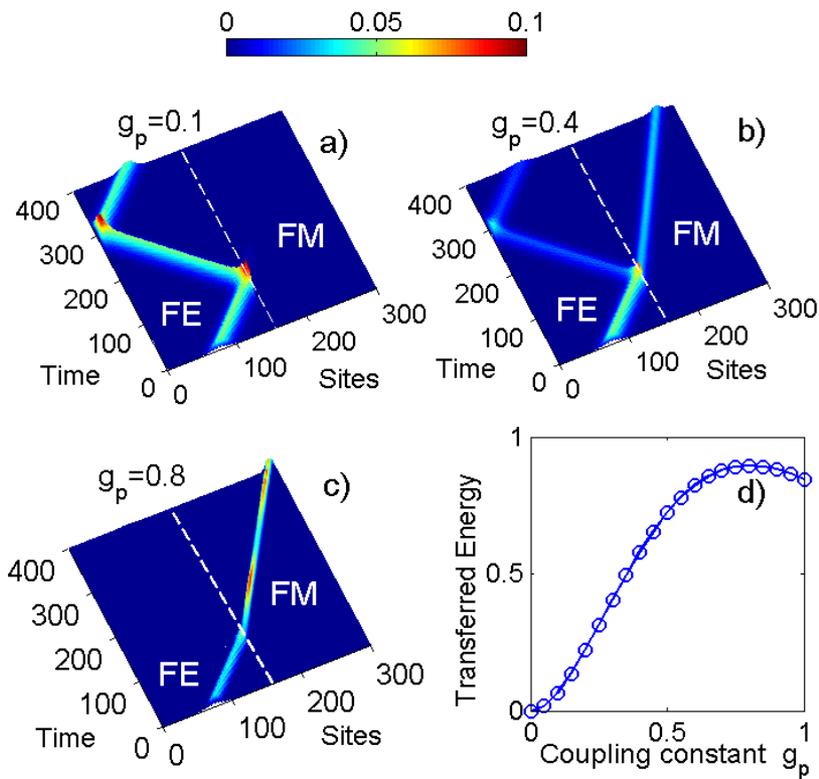
$$\begin{aligned}
 H &= H_P + H_S + V_{ME}, \\
 H_P &= \sum_{n=1}^N \left(\frac{1}{2} \frac{dP_n^2}{dt^2} + \frac{\alpha^{FE}}{2} P_n^2 + \frac{\beta^{FE}}{4} P_n^4 + \frac{1}{2} (P_{n+1} - P_n)^2 - E P_n \right) \\
 H_S &= \sum_{k=N+1}^M \left(-J \vec{M}_k \cdot \vec{M}_{k+1} - D (M_k^z)^2 - B M_k^z \right) \\
 V_{ME} &= -g_1 (P_N M_{N+1}^z) - g_2 (P_N M_{N+1}^z)^2,
 \end{aligned}$$

R. Ramesh and N. Spaldin Nature **6**, 21 (2007); M. Fiebig J. Phys. D: Appl. Phys. **38** R123 (2005)

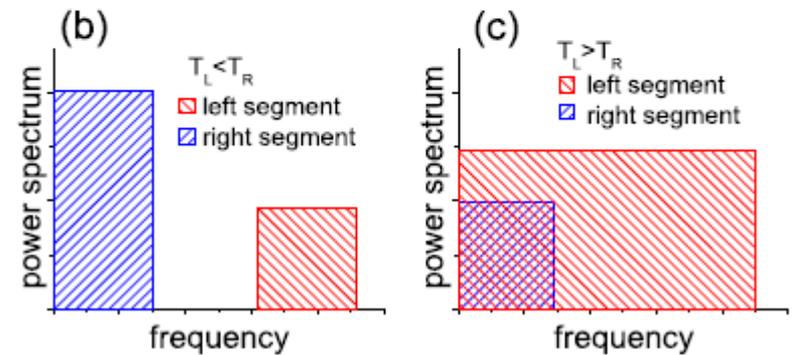
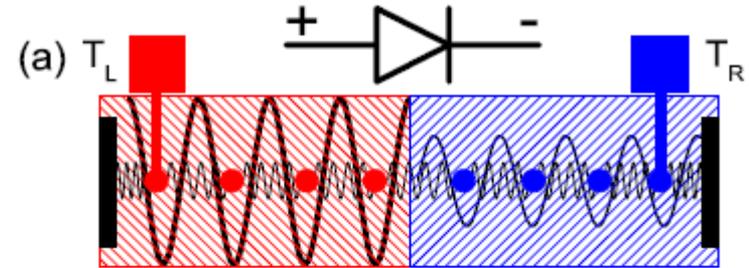
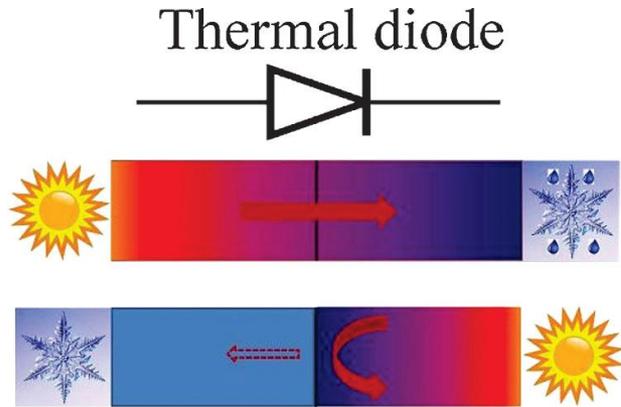
Soliton solutions

$$\begin{aligned}
 p_n &= \sum_{\alpha=1}^{\infty} \varepsilon^\alpha \sum_{m=-\infty}^{\infty} \Psi_m^{(\alpha)}(\xi, \tau) e^{im(\omega t - pn)}; & \xi &= \varepsilon(n - vt); & \tau &= \varepsilon^2 t, \\
 \frac{\partial}{\partial t} \Psi_m^{(\alpha)} &= -\varepsilon v \frac{\partial}{\partial \xi} \Psi_m^{(\alpha)} + \varepsilon^2 \frac{\partial}{\partial \tau} \Psi_m^{(\alpha)}; & \frac{\partial}{\partial n} \Psi_m^{(\alpha)} &= \varepsilon \frac{\partial}{\partial \xi} \Psi_m^{(\alpha)}, \\
 p_n &= \frac{A \cos[\omega_p t - q_p n + \delta \omega_p t]}{\cosh[(n - V_p t) / \Lambda_P]}, & s_k^\pm &= \frac{B e^{\pm i(\omega_s t - q_s k + \delta \omega_s t)}}{\cosh[(k - V_s t) / \Lambda_S]}, \\
 \omega_p &= \sqrt{\alpha + 2(1 - \cos q_p)}, & \omega_s &= 2[D + J(1 - \cos q_s)], \\
 \Lambda_P &= \frac{1}{A} \sqrt{\frac{2(\omega_p^4 - \alpha^2 - 4\alpha)}{3\omega_p^2 \beta}}, & \Lambda_S &= \frac{1}{B} \sqrt{\frac{4J \cos q_s}{\omega_s}}, \\
 \delta \omega_p &= A^2 \frac{3\beta}{16\omega_p}, & \delta \omega_s &= -B^2 \frac{\omega_s}{4}, & \omega_p + \delta \omega_p &= \omega_s + \delta \omega_s, \\
 \omega_s - \omega &= \left(\frac{g_p^2 \omega}{4} + \frac{3\beta}{16\omega} \right) A_{cr}^2.
 \end{aligned}$$

Transfer of the soliton through the interface



Thermal diode



Power spectra between left (L) and right (R) parts

$$S = \frac{\int_0^{\infty} P_L(\omega) P_R(\omega) d\omega}{\int_0^{\infty} P_L(\omega) d\omega \int_0^{\infty} P_R(\omega) d\omega}$$

The interface thermal resistance (Kapitza resistance)

$$R_+ = \frac{\Delta T}{J_+}, \quad \Delta T = |T_L - T_R|, \quad T_L - T_R > 0$$

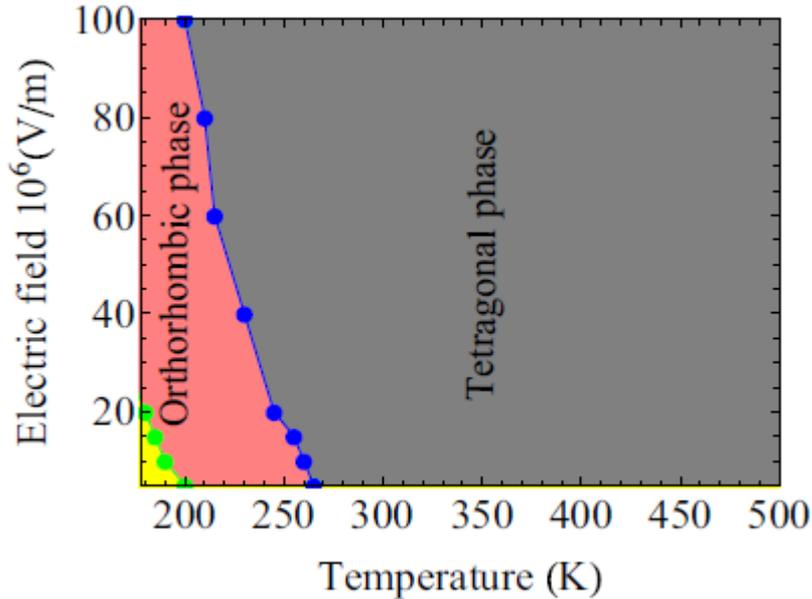
$$R_- = \frac{\Delta T}{J_-}, \quad \Delta T = |T_L - T_R|, \quad T_L - T_R < 0$$

$\frac{R_+}{R_-}$ = measures the rectification effect

N. Li, J. Ren, L. Wang, G. Zhang, P. Hänggi, and B. Li, Rev. Mod. Phys. **84**, 1045 (2012).

Advantage of the electric field

a) Tetragonal phase can be enlarged



b) Ferroelectric frequency spectrum can be controlled

$$\omega_{FE}(E) = \left\{ 4\alpha^{FE} \cos^2 \left[\cos^{-1} \left(\frac{3|E|}{2\alpha^{FE}} \sqrt{\frac{3\beta^{FE}}{\alpha^{FE}}} \right) / 3 \right] - \alpha^{FE} \right\}^{1/2}$$

Optimal electric field

$$E = \left| \frac{2\alpha^{FE}}{3} \sqrt{\frac{\alpha^{FE}}{3\beta^{FE}}} \cos \left[\frac{3}{2} \arccos \left(\frac{4D^2 - \alpha^{FE}}{2\alpha^{FE}} \right) \right] \right|$$

$$E = 3.4 \times 10^4 \text{ (V/sm)}$$

$$H = H_P + H_S + V_{ME},$$

$$H_P = \sum_{n=1}^N \left(\frac{1}{2} \frac{dP_n^2}{dt^2} + \frac{\alpha^{EF}}{2} P_n^2 + \frac{\beta^{EF}}{4} P_n^4 + \frac{1}{2} (P_{n+1} - P_n)^2 - EP_n \right)$$

$$H_S = \sum_{k=N+1}^M \left(-J_1 \vec{M}_k \vec{M}_{k+1} - D (M_k^z)^2 - BM_k^z \right)$$

$$V_{ME,m} = -g_m (P_N M_{N+1}^z), \quad g < J_2 < J_1$$

Equations of motion

Ferroelectric, part in tetragonal phase

$$\begin{aligned}\frac{dp_n}{dt} &= q_n, \\ \frac{dq_n}{dt} &= \alpha^{FE} p_n - \beta^{FE} p_n^3 - (2p_n - p_{n+1} - p_{n-1}) + E + \\ &g_1 M_1^z \delta_{nN} + 2g_2 p_n (M_1^z)^2 \delta_{nN} - \gamma_n q_n \delta_{1n} + \xi_n \delta_{1n}, \\ \langle \xi_n(t), \xi_m(t') \rangle &= 2\gamma_m T_m \delta(t-t'), \quad m = 1, \dots, N\end{aligned}$$

Ferroelectric, part **heat current**

$$\begin{aligned}\frac{\partial h_{k,k+1}}{\partial t} &= i [H_s, h_{k,k+1}], \\ J_k^H &= i [h_{k+1,k}, h_{k,k-1}], \\ H_s &= \sum_{k=N+1}^M \left(-J \vec{M}_k \vec{M}_{k+1} - D (M_k^z)^2 - B M_k^z \right).\end{aligned}$$

Ferromagnetic part

$$\begin{aligned}\frac{d\vec{M}_k}{dt} &= -\frac{1}{1+\alpha_k^2} \vec{M}_k \times \left(\vec{B}_k^{eff} + \alpha_k \vec{M}_k \times \vec{B}_k^{eff} \right), \\ \alpha_k &= \alpha \delta_{kM}, \quad \vec{B}_k^{eff} = \frac{\partial H}{\partial \vec{M}_k} + \delta_{kM} \vec{\eta}_k, \\ \langle \eta_k^i(t), \eta_k^j(t') \rangle &= 2\alpha_k T_k \delta_{ij} \delta(t-t'), \\ k &= N+1, \dots, M\end{aligned}$$

Ferromagnetic part **heat current**

$$\begin{aligned}J_k^H &= -\langle \dot{p}_k (p_{k+1} - p_k) \rangle \\ T_k &= \left(\frac{dp_k}{dt} \right)^2\end{aligned}$$

Inverting the thermal bias

$$\Delta \rightarrow -\Delta$$

$$T_1 = T_0(1 + \Delta), \quad T_M = T_0(1 - \Delta)$$

$$T_1 - T_M = 2T_0\Delta$$

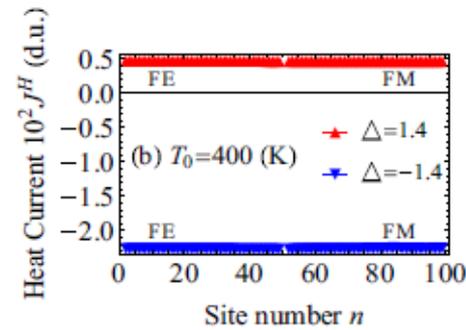
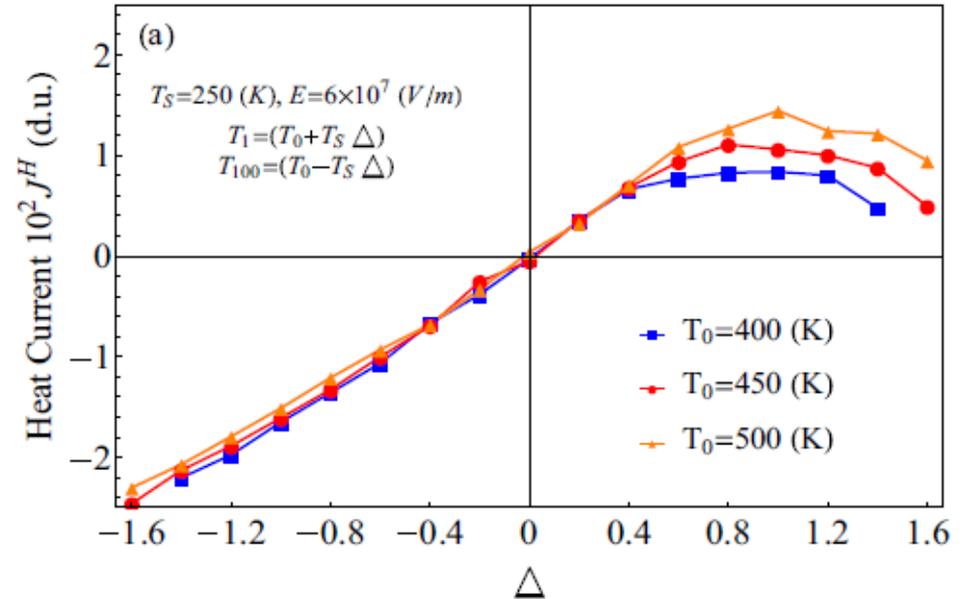
We observe asymmetry

$$\Delta \rightarrow -\Delta$$

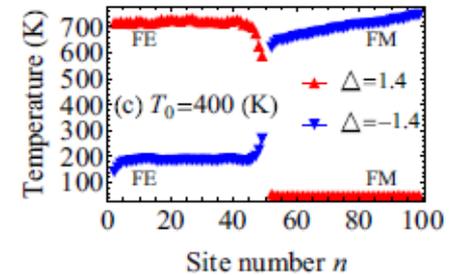
Temperature profiles are calculated self-consistently

$$M_k^z = L \left(\frac{M_k^z B_k^{eff}}{T_k} \right)$$

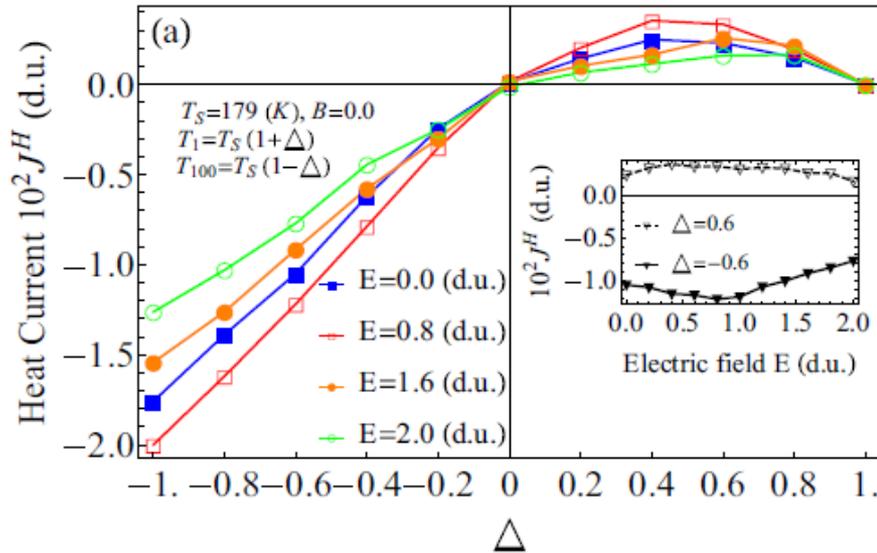
$$T_k = \left(\frac{dp_k}{dt} \right)^2$$



Heat currents



Temperature profiles



Heat current for different electric fields:
Optimal electric field

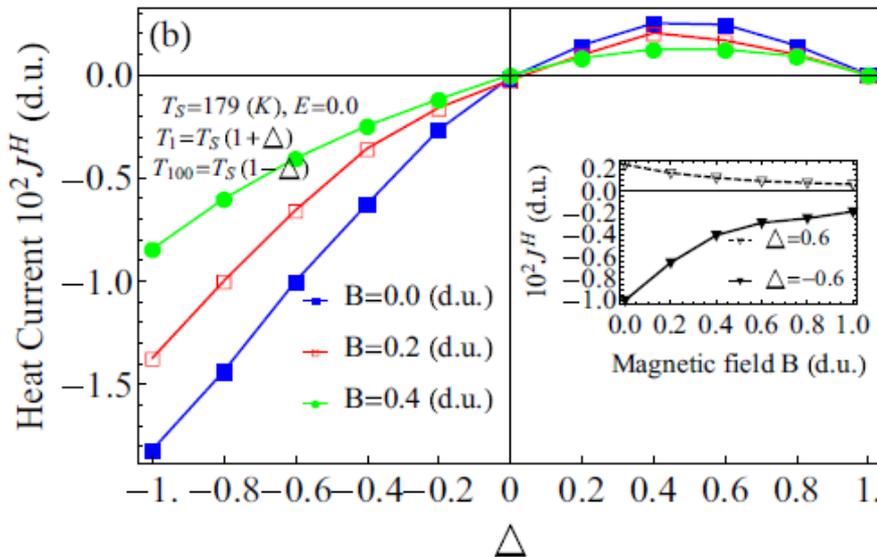
$$E=3.4 \times 10^4 \text{ (V/sm)}$$

Rectification

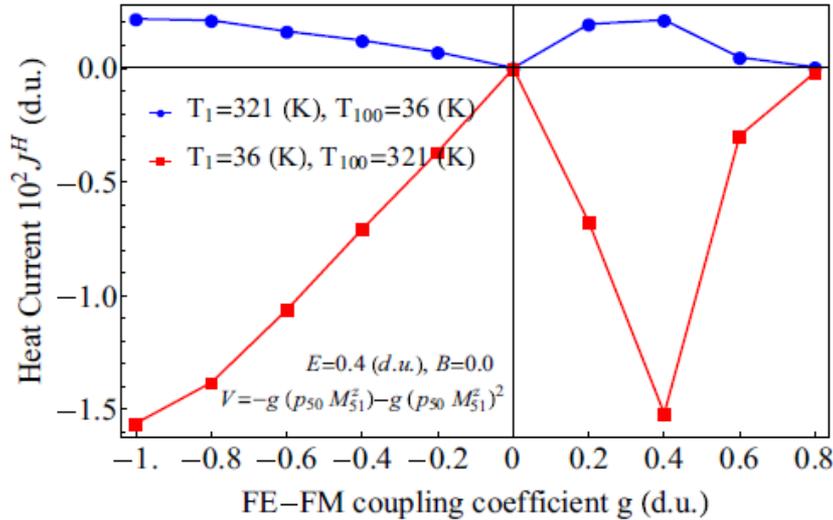
$$R_+ = \frac{\Delta T}{J_+}, \quad \Delta T = |T_L - T_R|, \quad T_L - T_R > 0$$

$$R_- = \frac{\Delta T}{J_-}, \quad \Delta T = |T_L - T_R|, \quad T_L - T_R < 0$$

$$\frac{R_+}{R_-} \approx 4$$



Heat current as a function of magnetoelectric coupling



We observe asymmetry

$g \rightarrow -g$

$$V_{ME} = -g \left(P_N M_{N+1}^z \right), \quad g > 0, \quad \Rightarrow \quad M_{N+1}^z \rightarrow 1$$

For large M_{N+1}^z current is suppressed

Parameters

Parameter	SI units	Dimensional unit (d.u.)
Bulk BaTiO ₃ single crystal		
P_0	0.265 C/m^2	$p_n = P_n/P_0$
α_1	$2.770 \times 10^7 \text{ V m/C}$	$\alpha^{\text{FE}} = \frac{\alpha_1}{\kappa} \approx 0.213$
α_2	$1.7 \times 10^8 \text{ Vm}^5/\text{C}^3$	$\beta^{\text{FE}} = \frac{\alpha_2 P_0^2}{\kappa} \approx 0.0918$
γ_v	$2.5 \times 10^{-5} \text{ V m s/C}$	$\gamma_m = \frac{\gamma_v \omega_0}{\kappa} \approx 0.192$
a_{FE}	$1.02 \times 10^{-9} \text{ m}$	
κ	$1.3 \times 10^8 \text{ V m/C}$	1
E	parameter (V/m)	$E \rightarrow \frac{1}{\kappa P_0} E \approx 3.4 \times 10^7 E$
T	parameter (K)	$T \rightarrow \frac{k_B}{\kappa P_0^2 a_{\text{FE}}^3} T \approx 1.4 \times 10^{-3} T$
J	joules/s	$J \rightarrow \frac{1}{\kappa P_0^2 \omega_0 a_{\text{FE}}^3} J \approx 10^8 J$
Bulk bcc Fe		
M_S	$1.71 \times 10^6 \text{ A/m}$	$\vec{s}_k = \vec{M}_k/M_S = (\vec{S}_k/S)$
γ	$1.76 \times 10^{11} \text{ (T s)}^{-1}$	
a_{FM}	$1.0 \times 10^{-9} \text{ m}$	
$\mu_S = M_S a_{\text{FM}}^3$	$1.71 \times 10^{-21} \text{ J/T}$	
α_{FM}	1.0	
K_1	$2.0 \times 10^6 \text{ J/m}^3$	$D = \frac{\gamma a_{\text{FM}}^3 K_1}{\omega_0 \mu_S} = 0.206$
A	$2.1 \times 10^{-11} \text{ J/m}$	$J = \frac{\gamma a_{\text{FM}} A}{\omega_0 \mu_S} = 2.16$
B	parameter (T)	$B \rightarrow \frac{\gamma}{\omega_0} B \approx 0.17 B$
T	parameter (K)	$T \rightarrow \frac{k_B \gamma}{\omega_0 \mu_S} T \approx 1.4 \times 10^{-3} T$
J	joules/s	$J \rightarrow \frac{\gamma}{\omega_0^2 \mu_S} J \approx 10^8 J$

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